Amendments to the Specification:

Please replace paragraph **[0004]** with the following rewritten paragraph:

[0004] Referring to the schematic views of Figs. 1A-1E in cross section illustrating major process steps of manufacturing a fine feldspathic earthenware in the prior art, the process steps include a step of placing a body on a so-called rollerhead machine 10 equipped with a gypsum mold, and press-forming the body into a plate-like or dish-like body. Fig. 1A shows this step. The thus formed bodies 12 each in the form of a plate or dish are dried for a sufficient time, and ~~is~~ are then biscuit-fired at a temperature of about 1100-1300°C in a kiln such that the formed bodies 12 are superposed on each other in a stack on a setter 14. Fig. 1B shows this step. Successively, each biscuit-fired body 16 is given an underglaze decoration, which is transferred from a transfer paper bonded to its surface or drawn with a suitable powdered pigment. Then, the biscuit-fired body 16 is supported by pins 18 at a plurality of positions (e.g., three positions) on its back surface, and the surfaces of the body 16 are uniformly coated with a glaze, with spray guns or sprayers 20. Fig. 1C shows this step. After the body 16 coated with the glaze is sufficiently dried, the body 16 is subjected to a glost firing ~~operating~~operation, with a refractory jig 22 as described in JP-U-54-4263. For example, this jig 22 is a generally annular structure having a plurality of projections 24 (e.g., three prismatic pins each in the form of a triangular prism having a length of a several tens of millimeter and three faces each having a width of several millimeters). The projections 24 protrude inwardly of the annular structure of the jig 22. The biscuit-fired body 16 is supported by the jig 22, with the projections 24 held in abutting contact with the back surface of the body 16. In this condition, the body 16 is glost-fired at a temperature of about 900-1200°C. Fig. 1D shows this step. Subsequently, the glost-fired fine feldspathic earthenware 26 is separated from the projections 24 of the jig 22. Usually, fragments 28 of the projections 24 adhere to the ~~earthenware 27~~earthenware 26 as a result of a reaction of the projections 24

with the glaze. These fragments 28 are removed with a grinding wheel 30 which carry a grinding layer formed of abrasives of diamond, silicon carbide or corundum. Fig. 1E shows this step. Thus, the fine feldspathic earthenware 26 is manufactured.

Please replace paragraph **[0005]** with the following rewritten paragraph:

[0005] Figs. 2A and 2B show in detail the step of removing the fragments 28 of the projections 24 which remain adhering to the fine feldspathic earthenware as a result of the reaction of the projections 24 with the glaze in the glost-firing step, after the glost-fired fine feldspathic earthenware 26 is removed from the projections 24 of the jig 22 described above. Fig. 2A shows the earthenware 26 before removal of the fragments 28, while Fig. 2B shows the earthenware 26 after the removal. The bottom plan view of Fig. 3 shows the fine feldspathic ~~earthenware 36~~ <u>earthenware 26</u> after the removal of the fragments 28. Fig. 2B is a cross sectional view taken along line 2-2 of Fig. 3. As shown in Figs. 2A, 2B and 3, the fine feldspathic earthenware 26 manufactured in the prior art process inevitably suffers from pin marks 32 caused by the pins 18 used to support the biscuit-fired body 16 in the glaze coating step, and ground spots 34 caused by the removal of the fragments 28 of the jig 22. These pin marks 32 and ground spots 34 have non-glazed surface areas which are not coated with the glaze and which have a relatively high water absorption percentage. In particular, the ground spots 34 have a comparatively large diameter of about 2-5mm, and accordingly give rise to various problems.

Please replace paragraph **[0024]** with the following rewritten paragraph:

[0024] Referring first to the bottom plan view of Fig. 4 and the fragmentary view of ~~Fig. 4~~ <u>Fig. 5</u> in cross section taken along line 5-5 of Fig. 4, there is shown a fine feldspathic earthenware (cream ware) 40 according to one preferred embodiment of the present invention.

As shown in Figs. 4 and 5, the fine feldspathic earthenware 40 is a dish having an outside diameter of about 170mm and a height of about 20mm, and has a comparatively large bottom portion. For example, this dish is used as a tableware. The fine feldspathic earthenware 40 includes a body 42 the body portion of which has an annular bottom 44 having an inside diameter of about 90mm, an outside diameter of about 100mm and a height of about 3mm. All surfaces of the body 42 are covered with a glaze layer 46, except an annular portion of the back surface which corresponds to the annular bottom 44. Namely, the glaze layer 46 is absent on a surface of the annular bottom 44 which has an almost semicircular shape in transverse cross section as shown in Fig. 5. The annular bottom 44 has an annular ridge having a diameter which is intermediate between the inside and outside diameters of the annular ~~portion~~ bottom 44. The surface of the annular ~~portion~~ bottom 44 which is not covered with the glaze layer 46 is covered with an annular vitrified layer 48 which has a lower water absorption percentage.

Please replace paragraph **[0025]** with the following rewritten paragraph:

[0025] The body 42 of the fine feldspathic earthenware 40 is formed of a composition which includes, as major components, silica (SiO_2), alumina (Al_2O_3), potassium oxide (K_2O) and sodium oxide (Na_2O), and other additives as needed, such as calcia (CaO) and magnesia (MgO). For example, the composition of the body 42 includes about 60-75% by weight of silica, about 15-25% of alumina, a total of about 2-5% by weight of sodium oxide and potassium oxide. To improve specific properties, for example, sinterability and formability of the composition, the composition may include desired additives such as calcium, magnesium and lithium ~~oxide~~oxides. The body 42 having the composition described above has a porous structure having a multiplicity of pores and a water absorption percentage of not lower than 3% and lower than 15%. To confirm that the body 42 has a water absorption percentage

within this specified range, the water absorption percentage of the body 42 is measured according to JIS R2205 which defines methods of measuring apparent porosity, water absorption percentage and specific gravity of refractory bricks.

Please replace paragraph **[0038]** with the following rewritten paragraph:

[0038] The body 42 coated with the glaze in the glaze coating step P11 is then subjected to wiping step P12, in which the glaze more or less applied to the surface of the annular bottom 44 is wiped off. ~~Fig. 7D~~Fig. 7E shows this wiping step P12. In the wiping step P12, the glaze is removed from the annular bottom 44, by a sponge 64. Preferably, the glaze is removed from the annular bottom 44 such that only the radially inner and outer end portions 48a, 48b (Fig. 5) of the semicircular surface of the annular vitrified layer 48 formed in the following glost-firing step P13 are covered with the glaze layer 46. That is, an almost entire area of the semicircular surface of the annular vitrified layer 48, except the radially inner and outer end portions 48a, 48b, is exposed to the atmosphere and is not covered by the glaze layer 46.

Please replace paragraph **[0039]** with the following rewritten paragraph:

[0039] The wiping step P12 to remove the glaze from the annular bottom 44 of the body 42 is followed by the glost-firing step P13 in which the body 42 is glost-fired so that the glaze layer 46 is formed on the surfaces of the body 42. Fig. 7F shows this glost-firing step P13. The body 42 is glost-fired at a temperature within a range of about 980-1160°C, while the body 42 placed on a setter 66 is held in a sagger (not shown). Although the annular bottom 44 of the body 42 is held in direct contact with the setter 66 during the glost-firing operation, the vitrified layer 48 formed so as to cover the annular bottom 44 is not fused to the setter 66 and can be easily separated from the setter 66, since the refractoriness of the

vitrified ~~layer 46~~ layer 48 is high enough to prevent the fusion of the vitrified ~~layer 46~~ layer 48 at the glost-firing temperature.